## THE ONE-TENTII PER CENT LEVEL OF THE RATIO OF VARIANCES

## By SUDHIR KUMAR BANERIEE

Fisher defines  $z = \log_{\bullet}(s_1/s_1)$ 

where  $s_1$  and  $s_2$  are the estimated standard deviations of two samples drawn from the same normal population. For a test of significance, therefore, one has to calculate the Naperian logarithm of the ratio of the two standard deviations (or what is the same thing, the difference between the Naperian logarithms of the two standard deviations). Finding the Naperian logarithms however takes time, and to avoid this, Mahalanobis published in 1932, 5 per cent and 1 per cent tables of  $s_1^*/s_2^*$  (and also of  $s_1/s_2$ ) and similar tables have also been given in G. W. Snedecor's book on the Analysis of Variance and Covariance. Now that C. G. Colcord and L. S. Deming are publishing a one-tenth per cent table of  $s_1$ , it will be convenient to have a table of one-tenth per cent values of  $(s_1^*/s_1^*)$  and  $(s_1/s_1^*)$  and  $(s_1/s_2^*)$  and  $(s_1/s_2^*)$  and  $(s_1/s_2^*)$  and  $(s_1/s_2^*)$  and  $(s_1/s_2^*)$ 

The present Table has been derived directly from Colcord and Deming's " One-tenth der cent Level of 2" in the following way: —

$$z = \frac{1}{2} \log_{\bullet} (s_1^3/s_2^2) = \frac{1}{2} \log_{\bullet} (x) = 1.1513 \log_{10} (x)$$

Thus

$$x = \text{Antilog}_{10} (z/1.1513) = \text{Antilog}_{10} 0.8686 (z)$$

The following example will illustrate the use of the Table. In a randomised block experiment the following analysis of variance was obtained.

	Mean Square	Ratio of Variance
Block 5	23-146	
Treatment 4	19-708	-
Error 20	2.725	7:23

Since the table has been constructed from the corresponding a table by Colcord and Deming, given correct to 4 places of decimals, the present table is correct within one unit in the fifth figure; but this will not in any way affect the usual test of agmificance of two observed variances.

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$$z = \frac{1}{2} \log_{4} (19.708/2.725)$$
  
= 1.1513 ( $\log_{10} 19.708 - \log_{10} 2.725$ )  
= 1.1513 × 0.8593  
= 0.9893

To test the significance, we have the following table:-

$$m_1 = 4$$
 and  $m_2 = 20$ 

	Values of z	Values of x
5:0 per cent 1:0 per cent 0:1 per cent	0.5265 (Fisher) -7443 ( ,, ) -9798 (Colcord & Demin	4:431 ( ,, )

Since the observed value of z (= 0.9893) exceeds not only the 1 per cent but also t. e. 0. Since the observed value of z given in Colcord and Deming's Table, the treatment is significant on the 0.1 per cent level.

The same result is reached more easily by calculating the ratio of variances and using the present Table. We have, in the present example,

$$x =$$
the ratio of variances =  $\frac{19.708}{2.725} = 7.23$ 

But 7:23 exceeds the 0:1 per cent value of the ratio of variances (7:102) given in the table, so that we seach the same conclusion almost immediately.

## REFERENCES

- Mahalanobis P. C. (1932):—Auxiliary Tables for Fisher's z-test in Analysis of Variance (Ind. Jour. Ag. Sc. Vol. II (6).
- Snedecor, G. W. (1934): —Calculation and Interpretation of Analysis of Variance and Covariance (Collegiate Press, Ames, Iowa.)

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DRE-TENTH PERCENT VALUES OF THE RATIO OF VARIANCE (s, 1/3,1)

		8		•	'n	٥	1	60	a	
-	.100901	.926661	23	562182	576375	.9062585	3923440.	.001865	.181.	8
3	<b>7.866</b>	0.666		000.5			2.660	9.666	9.600	
	167.46	148.5		187.08		_	131.57	9.061	1.80.87	_
•	24 126	827.19		123.4:Ju			859.64	160.87	143.71	
5	650.44	26.612	33.501	31.082		23.838	28.168	27.634	757.72	26.018
٠	\$5.200	86.02	23.702	21.802	\$0.8U	50.07	19.464	650.61	989.81	
1	616.66	21.688	18 77.2	17.188	16.206	15.37	15.0.0	10.01	17.3.4	
00		18.493	8.8.8	14.383	19:105	85×.7-1	101.7.1	170.71	8:1.11	
a		16.385	13.501	195.61	11:11	11.1.52	10.697	0:0:01	8 6	
2	31.030	14.306	12.553	11.282	[84.0]	120.0	R15.0	102.6	8.623	8.133
=		13.813	11.560	10.316	9.577	0.011	8.635	9.826	8.116	
2	_	1:2.07:2	10.803	0.633	3.805	8.318	8.001	7.711	7 450	
2		12.312	10-208	0.02	8.371	7.835	254.1	507.5	6.982	
=		11.780	0.230	8.073	7.0.2	7.438	1.078	6.802	2.89.9	
2	16.586	11.338	0.935	8.253	1.901	1.095	6.741	0.410	0.236	
.90	_	10.020	0.003	2.618	7-272	108.9	9.160	\$61.9	8.043	
12	_	10.639	27.7.8	1.033	2.0.2	6.563	6.773	2.963	5.753	
-	_	0×8.01	2K4.8	439	6.807	538.9	0.05	2.163	877.9	
2		10.157	0.7.9	1.761	909.9	921.9	518.5	0.5.0	5 387	
9	14-820	1.052	8G.08	7.102	191.9	810.9	2.69.5	2.410	5.5:40	\$.0.5
21		0.773	7.037	910.9	6.318	5.880	5.525	5.308	3.169	
ij		719.6	964.4	6.814	6.192	5.758	81.7.5	2.190	\$10.0°	
27		0.100	699.4	6.693	6.010	3.614	6.330	3.0%	CNN.+	
5	_	D.X.G	7.555	GNS.9	9.0.9	5.550	\$1.23	160 +	4.104	XX:3. *
23	13.875	6.5.7.6	7.450	6.493	\$.843	29.8	2.149	4.907	4.713	
26		0.110	7.356	901.9	5.802	5.345	6.003	679.7	169.1	
2		0.0.6	7.17.1	9.3.9	5.7.56	8.308	G50.T	4.739	1.203	
7.8		8.030	101.2	6.733	9.0.9	9.510	4.1122	169.1	\$1.30.5	
30	_	8.873	1.1.1	G. 187	635.9	8.120	1.876	\$19.7	4.77	
8	13.707	8.77.4	1.031	121.9	\$1533	3.127	4.817	185.9	DGE.T	
9	15.611	8.251	009.9	869.8	5.128	4.731	987.4	4.507	170.7	
3		7.765	0.172	5.307	4.757	4.873	WNO.7	3.H65	S.U.S	
120		7.31.2	8.703	250.7	4.415	110.7	3.765	3.516	20.8	C

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ONE-TENTIL PERCENT VALUES OF THE RATIO OF VARIANCES (817/813)-Could,

$\neg$	1			
	636483° 016°4 123°40 41°052 23°763	15.746 11.055 9.355 7.618 6.762 5.998 5.419 4.007 4.507 1.501	4.059 8.850 8.878 8.878 8.257 8.151 8.958	2'850 2'754 2'754 2'754 2'754 2'754 1'856 1'856
320	683942* 099*4 124*01 44*888	15:087 9:335 8:001 6:943 6:174 5:303 5:189 5:775	6.728 8.847 8.648 8.546 8.546 8.312 8.323 8.137	8 057 2.900 2.925 2.925 2.138 2.138 2.138 2.138
99	631286" 698"4 124"40 447743 21.332	16.216 12.119 9-728 8-128 8-189 7-123 5-763 5-763 5-763 6-189 4-639	4.388 4.177 8.708 8.708 8.738 8.738 8.286 8.286	3.216 3.082 3.023 2.971 2.237 1.032
3	628610* 999*4 124*96 45 080 24*050	10 444 12.522 10.722 17.268 6.518 6.518 5.927 5.467 5.467	84.13 84.13 84.13 81.83 81.83 81.83 84.84 84.84	8.253 8.175 8.175 8.172 8.172 8.172 8.172
Values of n,	626506* 099*4 125*48 45*430 2**883	16:653 19:231 10:113 89:517 7:460 6:634 6:630 5:256 4:050	4.607 4.184 4.1801 4.1.05 4.005 8.883 8.777 8.501 8.501	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
	623381* 090*4 123*94 43*768 25*1-43	16'801 12'733 10'302 6'723 7'637 6'847 6'248 5'103	4.846 4.246 4.150 4.150 4.026 8.1918 8.8922 8.8922 8.8922 8.8922	8 . 557 8 . 558 8 . 467 8 . 467 8 . 467 8 . 694 8 . 69
02	620893° 126°41 140°4 25°896	17.119 12.033 10.455 8.838 7.802 7.008 6.404 5.537 5.238	4.902 4.509 4.527 4.127 4.167 4.058 8.051 8.818	81772 81508 81508 81508 81508 8160 8170 8170 8170 8170 8170 8170 8170 817
22	615699* 999*4 127*35 46*758 25*909	17:359 10:324 10:329 6:129 6:129 6:709 6:709 6:709 6:709 6:231 5:246	5.274 4.704 4.704 4.302 4.437 4.337 4.139	8 1038 8 1030 8 1030 8 1733 8 1733 8 1717
71	610549° 899'6 128'30 47'407 26'416	17.039 11.194 11.194 6.570 8.445 7.623 7.003 6.130 6.130	5.518 5.824 5.937 4.697 4.697 4.583 4.893 4.893	4.238 4.170 4.100 4.000 4.000 8.642 8.818 8.918
		8+860 E2845	2222 2222 22222 22222	2 22222 483 2 22222 483